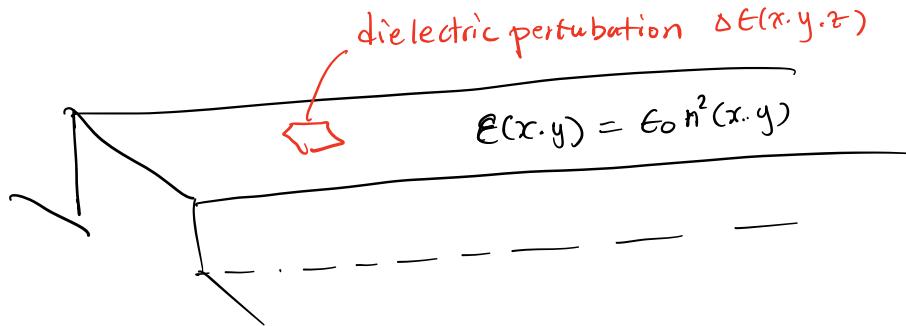


Lecture 8. Waveguide devices

Learning objectives:

- ① Mode coupling
- ② Waveguide coupling (directional coupler)
- ③ Ring resonator and critical coupling

1. Mode coupling (Yariv P603)



when $\epsilon(x,y)$ is independent of (z) , modes are independent
but when dielectric perturbation is applied to the waveguide,
(bending, surface corrugation), the modes are coupled together.

Eg. incident TE₀ mode, some of its power will be transferred to other modes, such as TE, TE₁...

Special case, $\Delta\epsilon(x,y,z) = \Delta\epsilon(x,y)$.

$$\epsilon(x,y) = \underbrace{\epsilon_a(x,y)}_{\text{dielectric const. of unperturbed WG.}} + \Delta\epsilon(x,y)$$

Let the unperturbed modes be

$$E_m = E_m(x,y) \cdot e^{i(\omega t - \beta_m z)}$$

where $\mathcal{E}_m(x,y)$ (transverse wavefunctions) satisfy

$$\nabla_t^2 \mathcal{E}_m(x,y) + [\omega^2 \mu \epsilon_a(x,y) - \beta_m^2] \mathcal{E}_m(x,y) = 0 \quad (1)$$

Apply the perturbation, we have

$$[\nabla_t^2 + \omega^2 \mu \epsilon_a(x,y) + \omega^2 \mu \Delta \epsilon(x,y)] (\mathcal{E}_m + \delta \mathcal{E}_m) = (\beta_m^2 + \delta \beta_m^2) (\mathcal{E}_m + \delta \mathcal{E}_m)$$

Neglect the second order term $\Delta \epsilon \cdot \delta \mathcal{E}_m$ and $\delta \beta_m^2 \delta \mathcal{E}_m$, use eq. (1), we have

$$[\nabla_t^2 + \omega^2 \mu \epsilon_a(x,y)] \delta \mathcal{E}_m + \omega^2 \mu \Delta \epsilon \mathcal{E}_m = \beta_m^2 \delta \mathcal{E}_m + \delta \beta_m^2 \mathcal{E}_m \quad (2)$$

To solve (2), we expand $\delta \mathcal{E}_m(x,y) = \sum_n a_{mn} \mathcal{E}_n(x,y)$

Plug in (2), we have

$$\sum_n a_{mn} (\beta_n^2 - \beta_m^2) \mathcal{E}_n(x,y) = (\delta \beta_m^2 - \omega^2 \mu \Delta \epsilon) \mathcal{E}_m(x,y) \quad (3)$$

Scalar-multiply (3) by \mathcal{E}_m^* , integral over x,y , use the orthogonal property.

i.e. $\int_A \mathcal{E}_m(x,y) \mathcal{E}_n^*(x,y) dx dy = 0,$

the left term is gone.

We get.

$$\iint \mathbf{E}_m^* \cdot (\delta \beta_m^2 - \omega^2 \mu_0 \epsilon) \mathbf{E}_m(x, y) = 0$$

$$\Rightarrow \delta \beta_m^2 = \frac{\iint \mathbf{E}_m^* \cdot \omega^2 \mu_0 \epsilon \mathbf{E}_m dx dy}{\iint \mathbf{E}_m^* \mathbf{E}_m dx dy}$$

Using the orthogonal relation: $\frac{\beta_m}{2\omega\mu} \iint \mathbf{E}_m^* \mathbf{E}_n dx dy = \delta_{mn}$.

$$\Rightarrow \delta \beta_m = \frac{\omega}{4} \iint \mathbf{E}_m^* \Delta \epsilon \mathbf{E}_m dx dy.$$

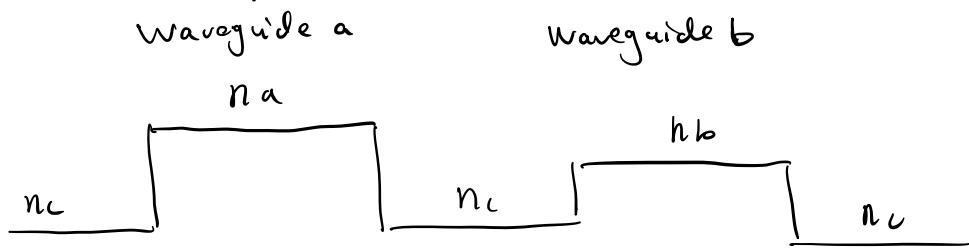
$$a_{mn} = \frac{\omega \beta_n}{2(\beta_m^2 - \beta_n^2)} \iint \mathbf{E}_n^* \Delta \epsilon(x, y) \mathbf{E}_m dx dy$$

$$a_{mm} = -\frac{\omega}{8 \beta_m} \iint \mathbf{E}_m^* \Delta \epsilon(x, y) \cdot \mathbf{E}_m dx dy$$

Define $K_{nm} = \delta \beta_m = \frac{\omega}{4} \iint \mathbf{E}_n^* \Delta \epsilon \mathbf{E}_m dx dy$.

as the "coupling coefficient" between modes.

2 - Waveguide coupling - Directional coupler.



Mode :

$$\mathcal{E}_a(x,y) e^{i(wt - \beta_a z)} \quad \mathcal{E}_b(x,y) e^{i(wt - \beta_b z)}$$

When they are closer (not too close!),
the general wave propagation in the coupled waveguide is

$$\vec{\mathbf{E}}(x,y,z,t) = A(z) \mathcal{E}_a(x,y) e^{i(wt - \beta_a z)} + B(z) \mathcal{E}_b(x,y) e^{i(wt - \beta_b z)}$$

Note:

- ① if distance between a. b is infinite,
 $A(z), B(z)$ do not depend on z ,

Index distribution $n^2(x, y)$

$$n^2(x, y) = \begin{cases} n_a^2 & \text{core a} \\ n_b^2 & \text{core b} \\ n_c^2 & \text{elsewhere} \end{cases}$$

$$\text{define } \Delta n_a^2(x, y) = \begin{cases} n_a^2 - n_c^2 & \text{core a} \\ 0 & \text{elsewhere} \end{cases}$$

$$\Delta n_b^2(x, y) = \begin{cases} n_b^2 - n_c^2 & \text{core b} \\ 0 & \text{elsewhere} \end{cases}$$

$$n_s^2(x, y) = n_c^2$$

The index profile: $n^2(x, y) = n_s^2(x, y) + \Delta n_a^2(x, y) + \Delta n_b^2(x, y)$

So, the wave equation for the composite waveguide:

$$\left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} + \frac{\partial^2}{\partial z^2} + \frac{\omega^2}{c} [n_s^2(x, y) + \Delta n_a^2(x, y) + \Delta n_b^2(x, y)] \right) \vec{E} = 0$$

where $\vec{E} = A(z) \vec{E}_a(x, y) e^{i(\omega t - \beta_a z)} + B(z) \vec{E}_b(x, y) e^{i(\omega t - \beta_b z)}$

Goal: solve $A(z), B(z)$!

Assuming slow variation of mode amplitudes over z , we get

$$\begin{aligned} & -2i\beta_a \frac{dA}{dz} \epsilon_a e^{i(\omega t - \beta_a z)} - 2i\beta_b \frac{dB}{dz} \epsilon_b e^{i(\omega t - \beta_b z)} \\ &= -\frac{\omega^2}{c^2} \Delta n_b^2(x,y) A \epsilon_a e^{i(\omega t - \beta_a z)} - \frac{\omega^2}{c^2} \Delta n_a^2(x,y) B \epsilon_b e^{i(\omega t - \beta_b z)} \end{aligned}$$

Take scalar product with $\epsilon_a^*(x,y)$ $\epsilon_b^*(x,y)$ and integrate over x,y plane, we get

$$\begin{aligned} \frac{dA}{dz} &= -i k_{ab} B e^{i(\beta_a - \beta_b)z} - i k_{aa} A. \\ \frac{dB}{dz} &= -i k_{ba} A e^{-i(\beta_a - \beta_b)z} - i k_{bb} B \end{aligned} \quad \left. \begin{array}{l} \text{④} \\ \text{Coupled mode} \\ \text{eq. (CME)} \end{array} \right\}$$

where $k_{ab} = \frac{\omega}{4} \epsilon_0 \iint \epsilon_a^* \Delta n_b^2(x,y) \epsilon_b dx dy$

$$k_{ba} = \frac{\omega}{4} \epsilon_0 \iint \epsilon_b^* \Delta n_b^2(x,y) \epsilon_a dx dy$$

$$k_{aa} = \frac{\omega}{4} \epsilon_0 \iint \epsilon_a^* \Delta n_b^2(x,y) \epsilon_a dx dy$$

$$k_{bb} = \frac{\omega}{4} \epsilon_0 \iint \epsilon_b^* \Delta n_a^2(x,y) \epsilon_b dx dy$$

Comments:

① k_{ab}, k_{ba} are exchange coupling between 2 waveguides

② k_{aa}, k_{bb} result from perturbation to one waveguide due to the presence of another

③ $K_{ab} = K_{ba}^*$, ensure the conservation of energy.

If assuming

$$E(x, y, z, t) = A(z) \epsilon_a e^{i(wt - (\beta_a + \kappa_{aa})z)} + B(z) \epsilon_b e^{i(wt - (\beta_b + \kappa_{bb})z)}$$

CME ④ reduces to

$$\begin{cases} \frac{dA}{dz} = -i K_{ab} B e^{i\gamma z} \\ \frac{dB}{dz} = -i K_{ba} A e^{-i\gamma z} \end{cases}, \quad 2\gamma = (\beta_a + \kappa_{aa}) - (\beta_b + \kappa_{bb}) \quad (5)$$

Assuming $K_{ab} = K_{ba} = K$, $s = \sqrt{k^2 + \gamma^2}$, solution of ⑤ is

$$\begin{cases} A(z) = A_0 e^{i\gamma z} \left(\cos s z - i \frac{\gamma}{s} \sin s z \right) \\ B(z) = -i A_0 e^{-i\gamma z} \frac{K}{s} \sin s z \end{cases}$$

In terms of power, $P_a(z) = |A(z)|^2$, $P_b(z) = |B(z)|^2$

$$\begin{cases} P_a(z) = P_0 - P_b(z) \end{cases} \quad (1)$$

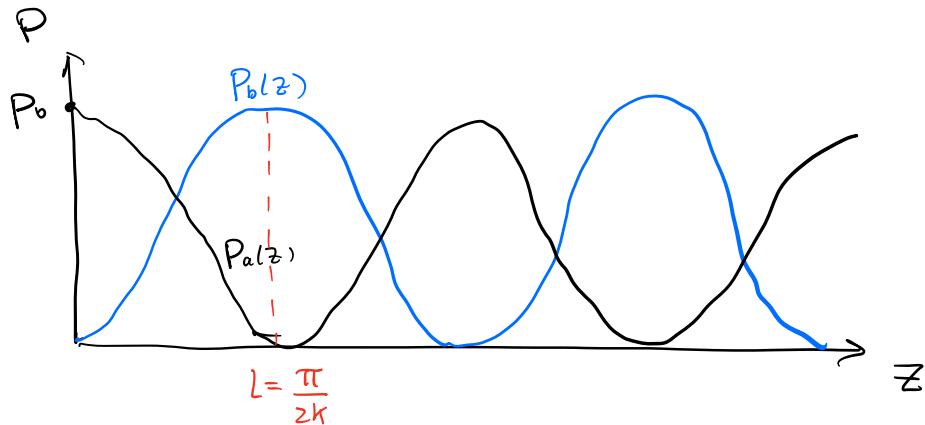
$$\begin{cases} P_b(z) = P_0 \frac{k^2}{k^2 + \gamma^2} \sin^2 \sqrt{k^2 + \gamma^2} z \end{cases} \quad (2)$$

where $P_0 = |A(0)|^2 = A_0^2$ is the input power at $z=0$

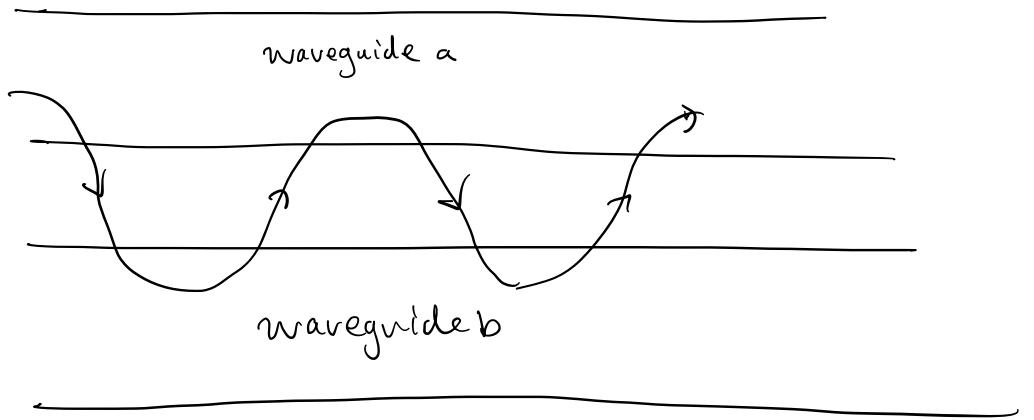
Comments

i) When $\gamma = 0$, ($\beta_a = \beta_b$), ② becomes

$$\left\{ \begin{array}{l} P_a(z) = P_0 - P_b(z) \\ P_b(z) = P_0 \sin^2 kz, \end{array} \right.$$



Directional coupler:



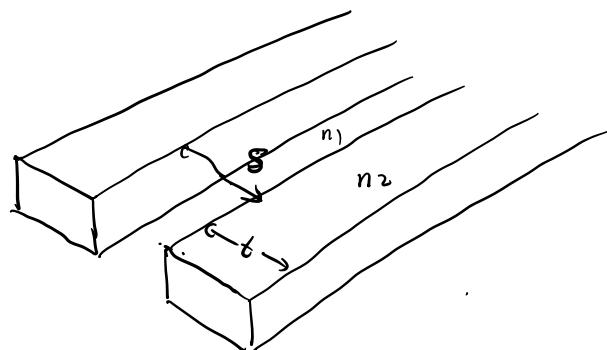
by controlling the coupling length L ,

we can control $|P_a(z)/P_b(z)|$

\rightarrow
 z

2) For $\delta \neq 0$, the maximum fraction of power that can be transferred is $\frac{\kappa^2}{\kappa^2 + \delta^2}$

For two identical channel waveguides



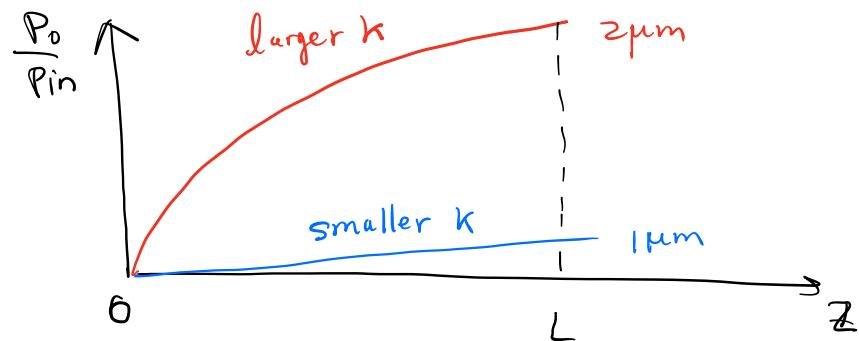
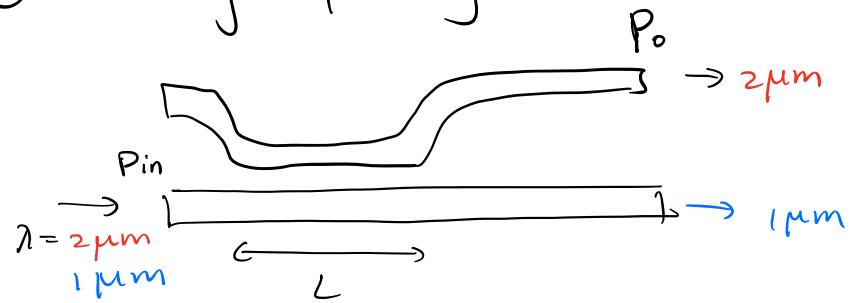
If modes are well confined ($t \gg 2q$)

$$\kappa = \frac{2h^2 q e^{-qs}}{\beta t (h^2 + q^2)} \left(\frac{2\pi}{\lambda} \right)^2 (n_2^2 - n_1^2)$$

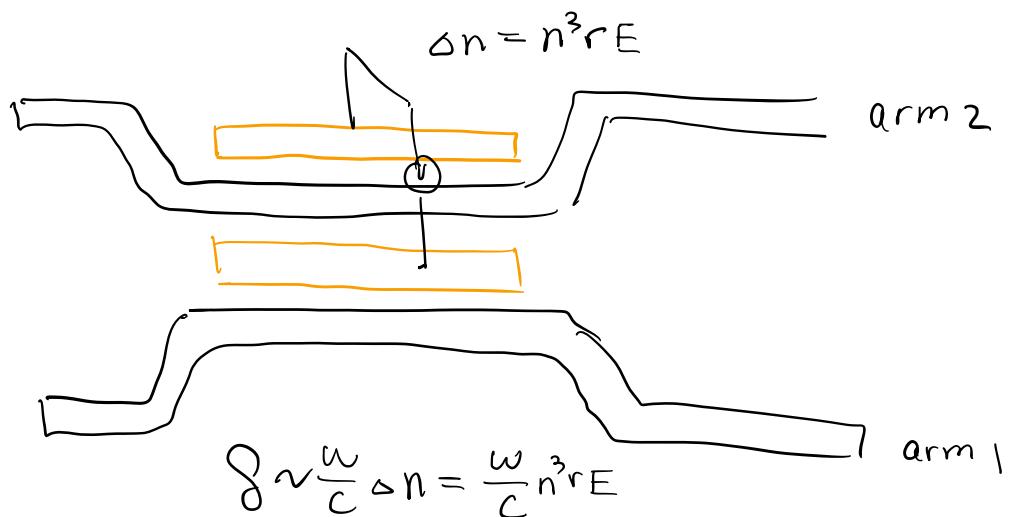
At $\lambda = 1 \mu\text{m}$, $t, s \sim 3 \mu\text{m}$, $\Delta n = 5 \times 10^{-3}$,
 $\kappa = 5 \text{ cm}^{-1}$, coupling length $L \approx k^{-1} = 2 \text{ mm}$.

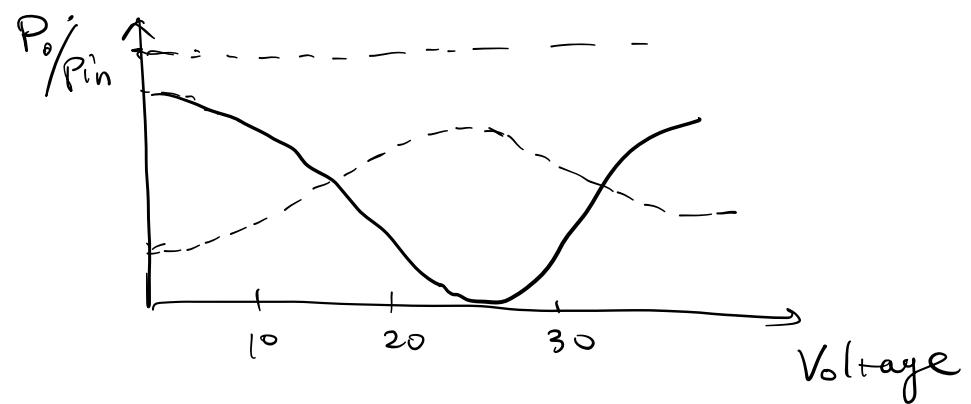
Applications

① Wavelength filtering



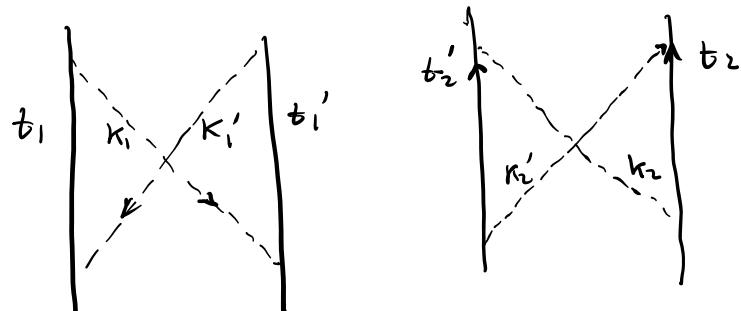
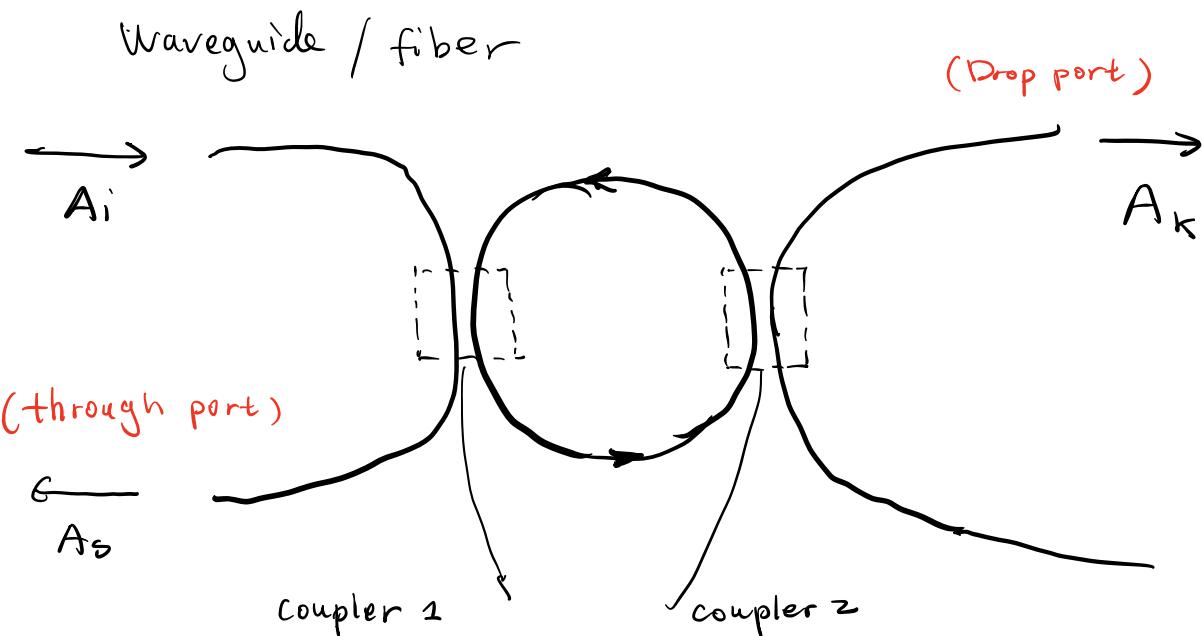
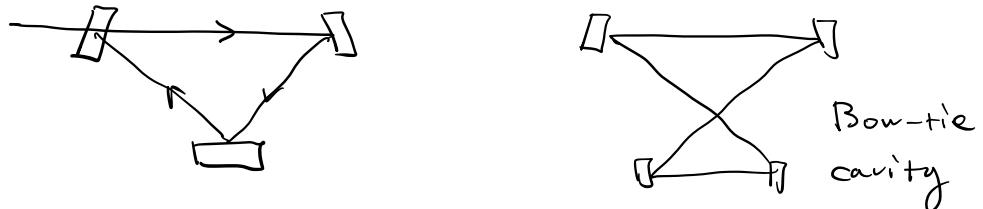
② Electro-optic switch





3. Ring resonators and critical coupling (Yariv, P185)

Free space ring resonators :



Define ① straight-through coupling coefficient t_1, t_1', t_2, t_2'

② cross-coupling coefficient k_1, k_1', k_2, k_2'

Model the ring as Fabry-Perot Etalon, Then,

$$A_s = t_1 A_i + k_1 k_1' t_2' e^{-i\delta} A_i + k_1 k_1' t_2' t_1' t_2' e^{-i\delta} + \dots$$

$$= \left\{ t_1 + k_1 k_1' t_2' e^{-i\delta} [1 + t_1' t_2' e^{-i\delta} + (t_1' t_2' e^{-i\delta})^2 + \dots] \right\} A_i$$

$$A_k = k_1 k_2' e^{-i\delta/2} [1 + t_1' t_2' e^{-i\delta} + (t_1' t_2' e^{-i\delta})^2 + \dots] A_i$$

where $\delta = \frac{2\pi n_{\text{eff}} d}{\lambda}$ circumference of the ring.

Summing up the geometric series .

$$\sigma = \frac{A_s}{A_i} = \frac{t_1 + (k_1 k_1' - t_1 t_1') t_2' e^{-i\delta}}{1 - t_1' t_2' e^{-i\delta}}$$

$$\chi = \frac{A_k}{A_i} = \frac{k_1 k_2' e^{-i\delta/2}}{1 - t_1' t_2' e^{-i\delta}}$$

When there is loss due to scattering, absorption and bending.

$$\sigma = \frac{A_s}{A_i} = \frac{t_1 + (k_1 k'_1 - t_1 t'_1) t'_2 e^{-i\delta} e^{-2d}}{1 - t'_1 t'_2 e^{-i\delta} e^{-2d}} \quad (\text{T from input to through})$$

$$\chi = \frac{A_n}{A_i} = \frac{k_1 k'_2 e^{-i\frac{\delta}{2}} e^{-2d}}{1 - t'_1 t'_2 e^{-i\delta} e^{-2d}} \quad (\text{T from input to drop})$$

which is quite similar to F-P etalon(cavity).

Q: How to determine (t, t'_1, t'_2, t'_1) and (k_1, k'_1, k_2, k'_2) ?

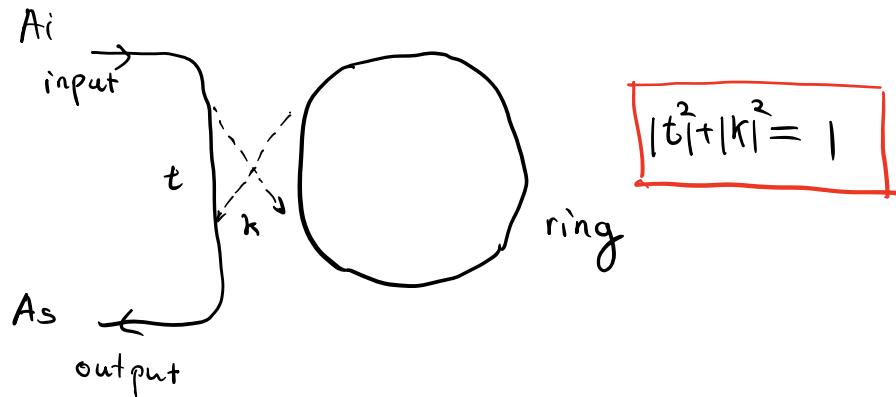
A: They are not independent of each other. They are related by reciprocity, conservation of energy and time-reversal symmetry.

$$\text{i.e. } \begin{cases} t_1^2 + k_1^2 = t'_1^2 + k'_1^2 = 1 \\ t_1 t'_1 - k_1 k'_1 = -1 \end{cases} \quad (\text{Yariv P, 186~188})$$

Then we have:

$$\sigma = \frac{t_1 + t'_2 e^{-i\delta} e^{-2d}}{1 - t'_1 t'_2 e^{-i\delta} e^{-2d}}$$

Assuming $k_2 = 0$, $t_2 = -1$, we have



$$\sigma = \frac{As}{Ai} = \frac{t_i - ae^{-i\delta}}{1 + t'_i a e^{-i\delta}} = \frac{t - ae^{-i\delta}}{1 - t^* a e^{-i\delta}}$$

where $t'_i = -t_i^* = -t^*$, $a = \exp(-2\alpha)$

$$|\sigma|^2 = \left| \frac{As}{Ai} \right|^2 = \frac{a^2 + t^2 - 2at \cos \delta}{1 + a^2 t^2 - 2at \cos \delta}$$

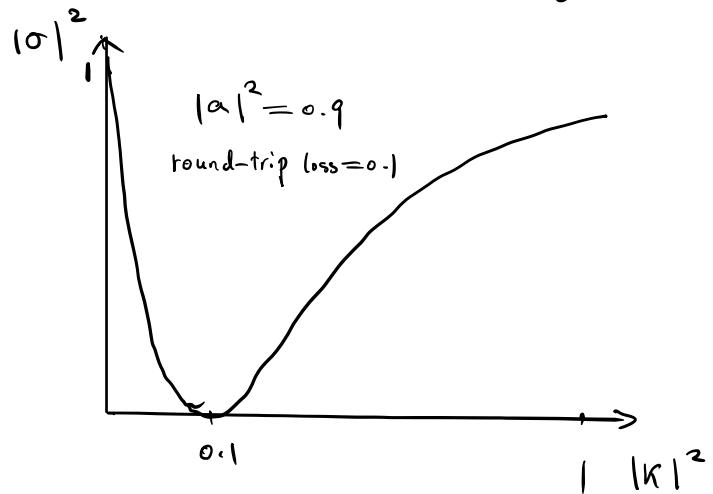
When at resonance ($\delta = 2m\pi$, $m = 1, 2, \dots$)

$$|\sigma|^2 = \left| \frac{As}{Ai} \right|^2 = \frac{(a-t)^2}{(1-at)^2}$$

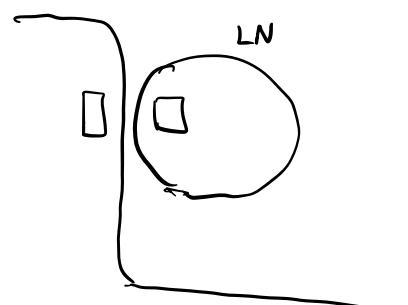
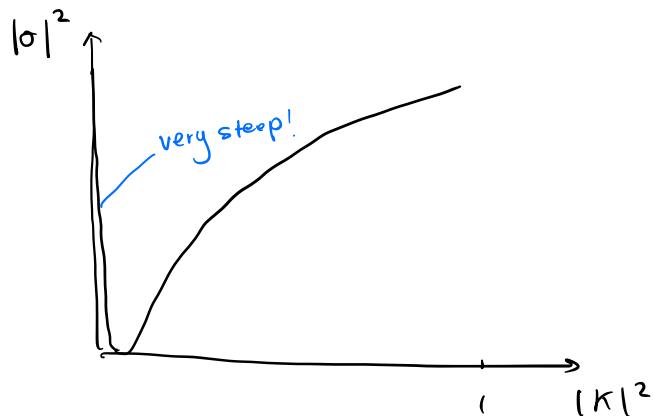
Comments:

① $|t|^2 \Rightarrow$ when $a = t = \sqrt{1 - |k|^2}$, i.e. $|k|^2 = 1 - |a|^2 = \text{round-trip loss}$

This is known as critical coupling condition



② For high Finesse, high Q-resonators, $|a| \sim 1$.
round-trip loss = $1 - |a| \approx 0$.



A small modulation of $|k|$ will modulate the transmission from zero to unity. \rightarrow Applications, high modulation depth modulators.