1. Review of OPA

$$CAE_{S}: \int \frac{dA_{1}}{dz} = \frac{2i\omega_{1}^{2}deff}{k_{1}c^{2}}A_{3}A_{1}^{*}e^{i\omega k^{2}}$$

Generic solution:

$$\begin{cases} A_{1}(2) = \left[A_{1}(0)\left(\cosh q 2 - \frac{i \delta k}{2q} \sinh q 2\right) + \frac{k_{2}}{q} A_{2}(0) \sinh q 2 \right] e^{\frac{i \delta k^{2}}{2}} \\ A_{2}(2) = \left[A_{2}(0)\left(\cosh q 2 - \frac{i \delta k}{2q} \sinh q 2\right) + \frac{k_{2}}{q} A_{1}(0) \sinh q 2 \right] e^{\frac{i \delta k}{2}} \\ \cosh q 2 - \frac{i \delta k}{2q} \sinh q 2 + \frac{k_{2}}{q} A_{1}(0) \sinh q 2 \right] e^{\frac{i \delta k}{2}} \\ \cosh q 2 - \frac{i \delta k}{2q} \sinh q 2 + \frac{k_{2}}{q} A_{1}(0) \sinh q 2 \right] e^{\frac{i \delta k}{2}} \\ \cosh q 2 - \frac{i \delta k}{2q} \sinh q 2 + \frac{k_{2}}{q} A_{1}(0) \sinh q 2 = \frac{i \delta k}{2} \\ \cosh q 2 - \frac{i \delta k}{2} \sinh q 2 + \frac{k_{2}}{q} A_{1}(0) \sinh q 2 = \frac{i \delta k}{2} \\ \cosh q 2 - \frac{i \delta k}{2} \sinh q 2 + \frac{k_{2}}{q} A_{1}(0) \sinh q 2 = \frac{i \delta k}{2} \\ \cosh q 2 - \frac{i \delta k}{2} \sinh q 2 + \frac{k_{2}}{q} A_{1}(0) \sinh q 2 = \frac{i \delta k}{2} \\ \cosh q 2 - \frac{i \delta k}{2} \sinh q 2 + \frac{k_{2}}{q} \cosh q 2 + \frac{k_{2}$$

Boundary conditions:  
() Non-degenerate OPA, 
$$A_{1}(0) = 0$$
 (no idler imput)

$$if \circ k = 0$$

$$\int A_{1}(z) = A_{1}(z) \cosh g z = \frac{1}{2} A_{1}(z) \exp(gz)$$

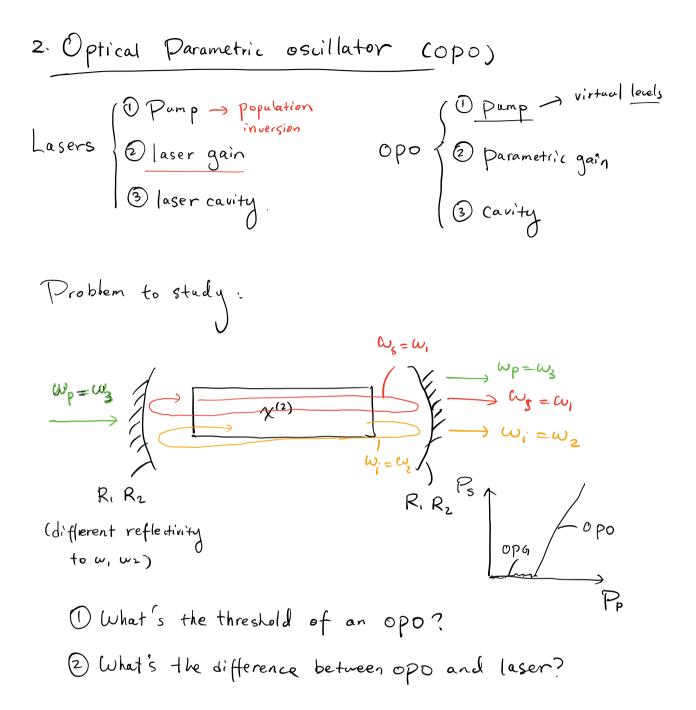
$$\int A_{2}(z) = i \left(\frac{n_{1}\omega_{2}}{n_{2}\omega_{1}}\right)^{2} \cdot \frac{A_{3}}{|A_{3}|} \cdot A_{1}^{*}(z) \sinh g z \longrightarrow A_{1}^{*}(z) \exp(gz)$$

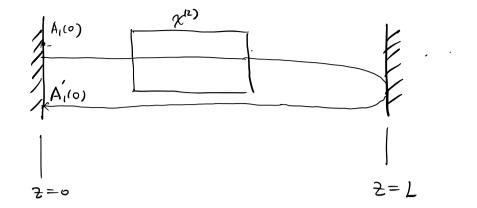
$$|A_{1}|^{2} \left(\frac{f \sin g}{|A_{1}|^{2}} + \frac{f \sin g}{|A_{1}|^{2}} + \frac$$

(2) Degenerate OPA: signal & idler are indistinguishable  

$$A_1(0) = A_{10} \cdot e^{i\phi_{10}} \neq 0$$
  
 $\Rightarrow A_2(2) = A_{10} e^{i\phi_{10}} \left[ \cosh(g_2) + e^{i(\phi_{20} - 2\phi_{10} + \frac{\pi}{2})} + \sinh(g_2) \right]$ 

phase - sensitive





General threshold condition  $(\delta k = 0)$ Yound trip gain = round trip loss Or  $A_1(0) = A_1(0)'$   $A_2(0) = A_2(0)'$   $= \frac{A_1(0)}{A_2(0)} = \left[A_1(0)\cosh g L + \frac{K_1}{g}A_2(0)\sinh g L\right](1-l_1) \odot$   $A_2^{*}(0) = \left[A_2^{*}(0)\cosh g L + \frac{K_2^{*}}{g}A_1(0)\sinh g L\right](1-l_1) \odot$   $A_2^{*}(0) = \left[A_2^{*}(0)\cosh g L + \frac{K_2^{*}}{g}A_1(0)\sinh g L\right](1-l_2) \odot$   $J_2 = 1-R_2e^{-\frac{3}{2}L}$  $l_1 \cdot l_2 \cdot are$  "fractional" amplitude loss per pass

ai is the absorption coefficient of the crystal at wi

Let () and (2) both satisfy.  

$$\Rightarrow \cosh g L = 1 + \frac{l_1 l_2}{2 - l_1 - l_2}$$

1 Doubly-resonant OPO (DRO):  
both Ws and W; are resonating in the cavity.  

$$\Rightarrow l_1 \ll 1$$
,  $l_2 \ll 1$   
 $\cosh gL \simeq 1 + \frac{1}{2}g^2L^2 = 1 + \frac{l_1l_2}{2-l_1-l_2}$   
 $\Rightarrow g^2L^2 = l_1l_2 = (1-R_1e^{-\lambda_1L})(1-R_2e^{-\lambda_2L})$ 

(2) Singly resonant OPO (SRO)  
Only signal is resonating, no feedback for idler, i.e. 
$$l_2 = 1$$
  
 $\cosh g L = 1 + \frac{l_1}{1 - l_1} \simeq \frac{1}{1 - l_1}$   
Assume  $l_1 \ll 1$ .  
 $1 + \frac{1}{2}g^2L^2 \simeq 1 + \frac{l_1}{(1 - l_1)} \gg 1$   
 $g^2L^2 = 2l_1 = 2 \cdot (1 - R_1e^{-21L})$ 

## Comments:

Threshold value of 
$$g_{L}$$
 for a SRO is larger than  
that of DRO by a factor of  $\int_{-\frac{1}{2}}^{\frac{1}{2}} |oss|$  of idlen  
in DRO

(2) There increase in threshold pumping intensity of the SRO to DRO is  $\left[\frac{(g+L)_{SRO}}{(g+L)_{DRO}}\right]^2 = \frac{2}{L_2}$ 

Example:  

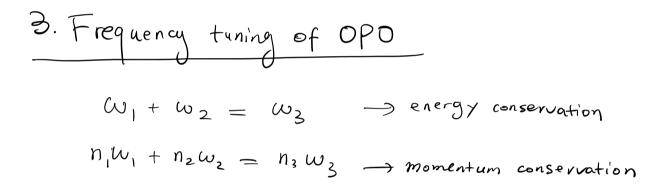
$$KTP: L = 10 \text{ mm}, \text{ deff} = 3 \text{ pm/V}, n_p = n_s = n_i = 1.5$$
  
 $P^{an}p: 1064 \text{ nm}, W_0 = 20 \mu \text{m}, \text{ signal} \sim 2.12 \mu \text{m}.$   
 $idler: 2.14 \mu \text{m}.$ 

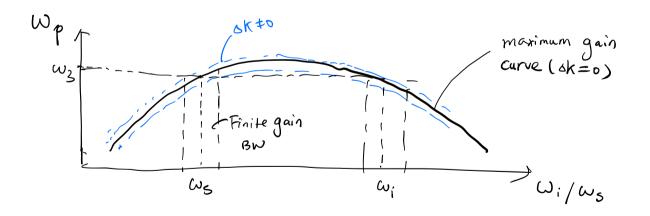
SRO:  

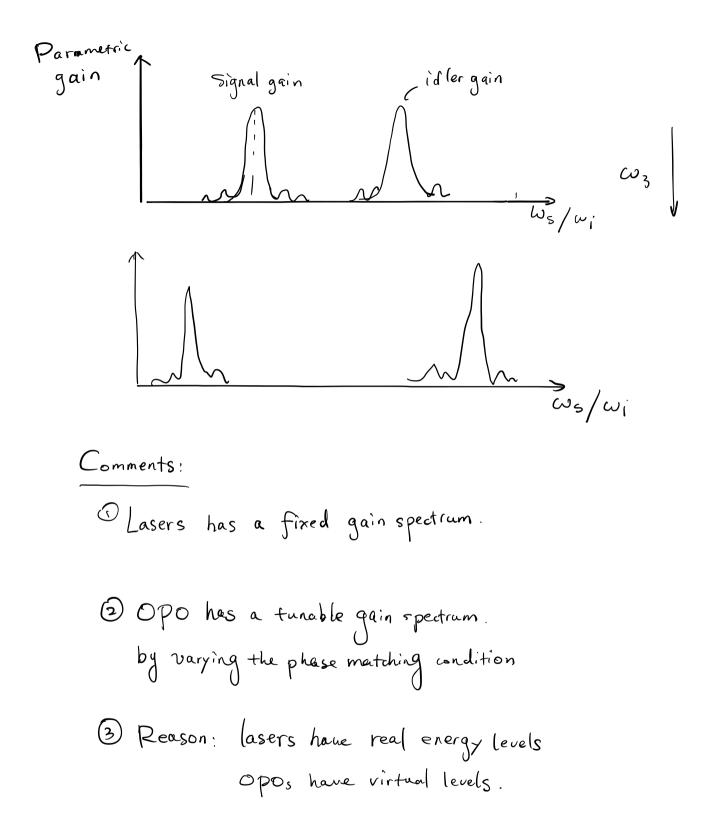
$$\frac{\partial s}{\partial s} = \frac{2^{\circ}}{0}.$$

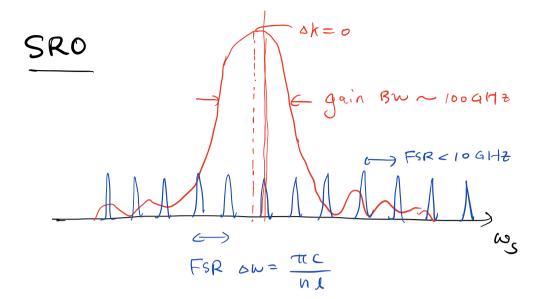
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If we tune the  $W_3$ , or phase matching condition. We can tune the oscillation frequency of the oppo. the resolution can be as high as the FSR. DRO  $\frac{ttc}{n!}$ 

() For, DRO, oscillation occurs when ws and its corresponding w; can both oscillate.

 $\Delta \omega = \frac{\pi c}{\ell(n_2 - n_1)}$ 

tic nul

osc. fras.

0

OSC. freq.

 $\omega_{i}$ 

3 Due to these constrains, DRO cannot be tuned continously.

( Not stable. 
$$\Delta W = \frac{\pi L/L}{n_2 - n_1} = \frac{n_2 - n_1}{n_2 - n_1} = \frac{n_2 - n_1}{n_2 - n_1} = \frac{1}{n_2 - n_1}$$
  
A small variation of cavity length, can induce a large  $\Delta W$ .

