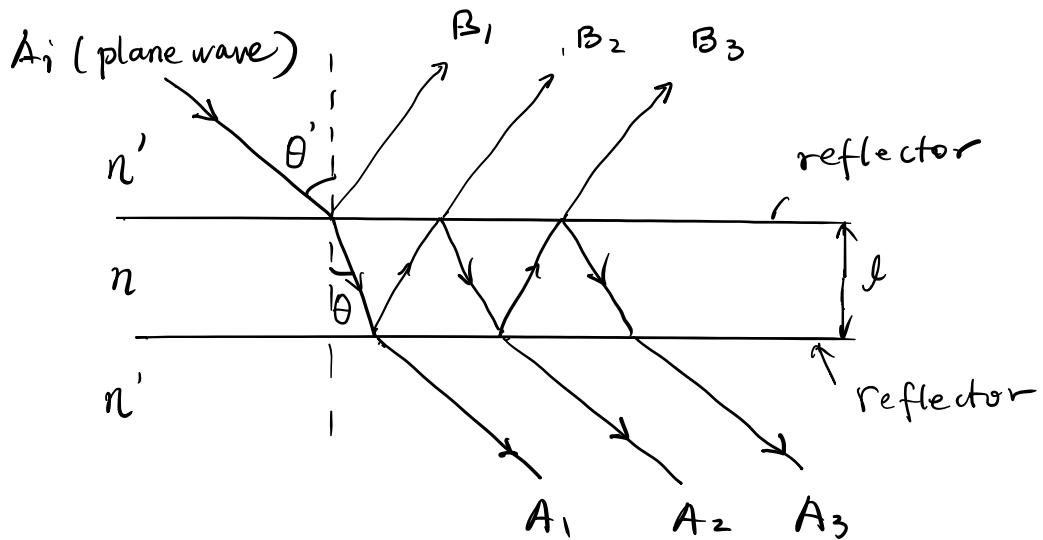


## Lecture 5: Thin-film optical devices

Learning objectives:

1. Symmetric Fabry-Perot etalon
2. Asymmetric .. .. ..
3. Finesse and quality (Q-) factor
4. Intracavity field
5. Multicavity etalons and transfer matrix

# 1. Symmetric Fabry-Perot etalon. (P161. Yariv)



$r$ : reflection coefficient of the interface  
 $t$ : transmission coefficient for waves incident from  $n'$  to  $n$   
 $r'$ : reflection ... ... ... ...  $n \text{ to } n'$   
 $t'$ : transmission ... ... ... ...  $n \text{ to } n'$

Reflected waves:

$$\begin{aligned}
 B_1 &= r A_i \\
 B_2 &= t t' r' A_i e^{-i\delta} - \text{phase shift} \\
 B_3 &= t t' r'^3 A_i e^{-i2\delta}
 \end{aligned}$$

Transmitted waves:

$$\begin{aligned}
 A_1 &= t t' A_i e^{-i\delta/2} \\
 A_2 &= t t' r'^2 e^{-i\delta} A_i e^{-i\delta/2} \\
 A_3 &= t t' r'^4 e^{-i2\delta} A_i e^{-i\delta/2}
 \end{aligned}$$

The total reflected wave:

$$A_r = [r + t t' r' e^{-i\delta} (1 + r'^2 e^{-i\delta} + r'^4 e^{-2i\delta} + \dots)] A_i$$

$$r' = -r = \frac{(1 - e^{-i\delta})r}{1 - r^2 e^{-i\delta}} A_i$$

$$R = r^2 = r'^2 = \frac{(1 - e^{-i\delta})\sqrt{R}}{1 - R e^{-i\delta}} A_i$$

Total transmitted wave

$$A_t = A_i t t' (1 + r'^2 e^{-i\delta} + r'^4 e^{-2i\delta} + \dots) e^{-i\frac{\delta}{2}}$$

$$T = t t', r^2 + t t'^2 = 1 = \frac{T e^{-i\frac{\delta}{2}}}{1 - R e^{-i\delta}} A_i$$

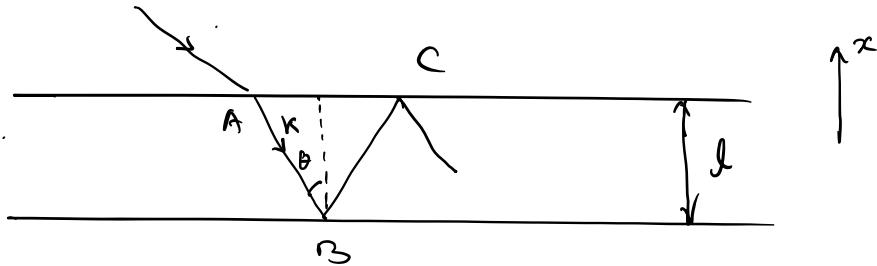
Intensity ratio:

$$\frac{I_r}{I_i} = \frac{A_r A_r^*}{A_i A_i^*} = \frac{4R \sin^2(\frac{\delta}{2})}{(1-R)^2 + 4R \sin^2(\frac{\delta}{2})}$$

$$\frac{I_t}{I_i} = \frac{A_t \cdot A_t^*}{A_i \cdot A_i^*} = \frac{(1-R)^2}{(1-R)^2 + 4R \sin^2(\frac{\delta}{2})}$$

Clearly,  $I_r + I_t = I_i$ , power is conserved.

Let's look into the phase shift ( $\delta$ )



One round trip:

$$\begin{aligned}\Delta L &= AB + BC = 2l \cos \theta \\ \Rightarrow \delta &= k \cdot \Delta L = n k_0 \Delta L = \frac{2\pi n}{\lambda} \cdot 2l \cos \theta = \frac{4\pi nl}{\lambda} \cos \theta \\ &= \underline{2k_x \cdot l}\end{aligned}$$

Summary:

Transmission  $\frac{I_t}{I_i} = \frac{(1-R)^2}{(1-R)^2 + 4R \sin^2(\frac{\delta}{2})}$  becomes unity

when  $\frac{\delta}{2} = m\pi$ ,

$$\text{i.e., } \delta = \frac{4\pi nl}{\lambda} \cos \theta = 2m\pi, \quad m = 1, 2, \dots$$

translate  $\lambda$  into frequency  $v$  using  $v = \frac{c}{\lambda}$ ,

$$v_m = m \frac{c}{2nl \cos \theta}, \quad m = 1, 2, \dots$$

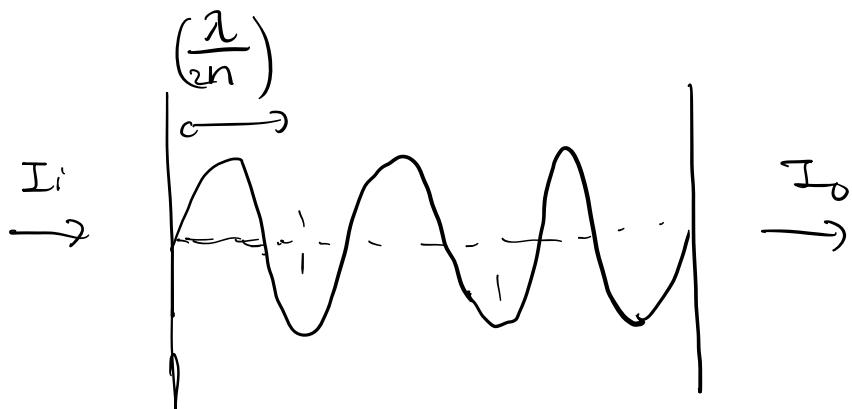
$$\text{or } l = m \left( \frac{\lambda}{2n \cos \theta} \right), \quad m = 1, 2, \dots$$

For normal incidence,  $\theta = 0^\circ$

Resonance condition:

$$v_m = m \cdot \frac{c}{2n\ell},$$

$$\ell = m \left( \frac{\lambda}{2n} \right),$$

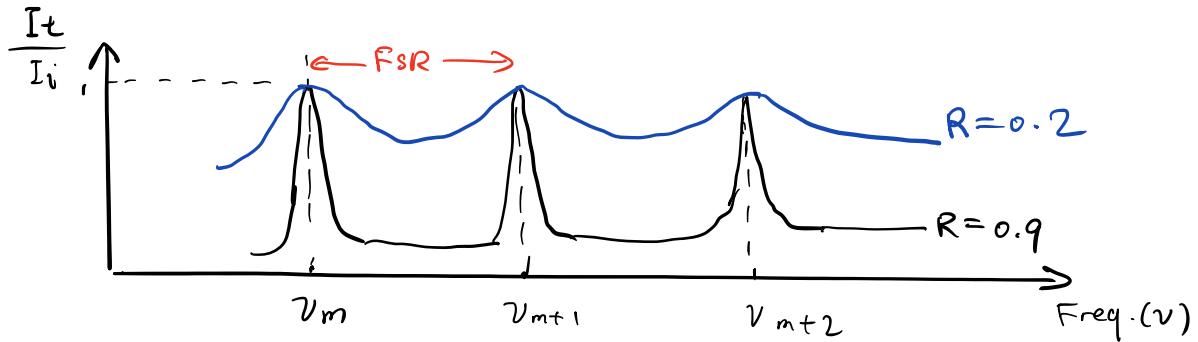


Physical meaning:

resonance happens when  $\ell$  is an integral number of half-wavelength.

② The transmission is unity at discrete  $\nu_m$ ,

$$\Delta\nu = \nu_{m+1} - \nu_m = \frac{c}{2nL\cos\theta} \quad \rightarrow \text{Free spectral range (FSR)}$$

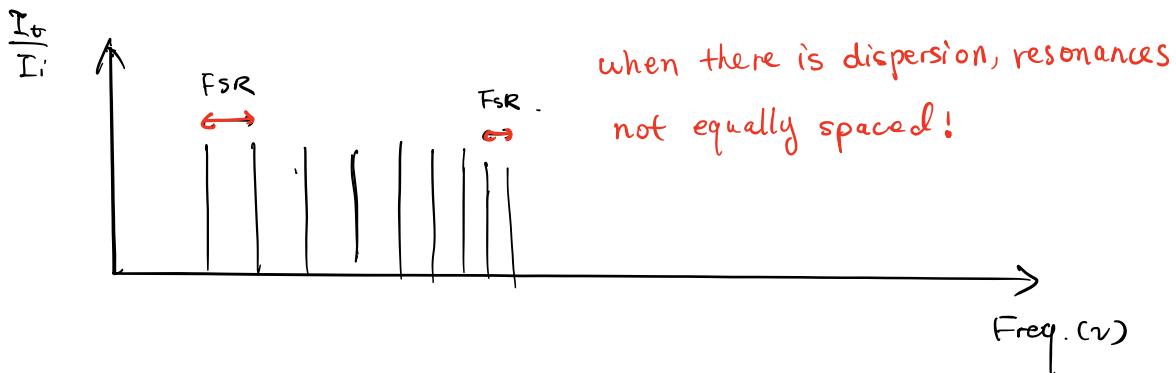


larger  $L$  leads to smaller FSR

- ③ ignore dispersion, FSR is a constant,  
with dispersion,

$$FSR = \Delta\nu = \nu_{m+1} - \nu_m = \frac{c}{2nL\cos\theta} = \frac{\nu_g}{2L\cos\theta_i}$$

Physical meaning:



④ When there is gain/loss, maximum transmission is not unity.  
(more usual cases)

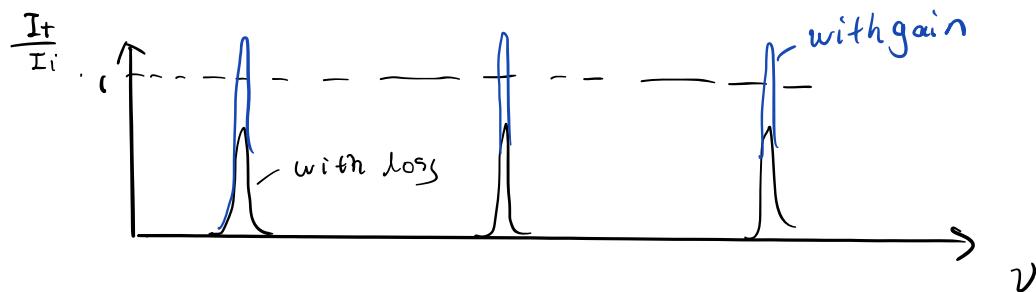
Define  $G = \exp(-\alpha l)$  as the intensity gain (or loss) per pass.

$\begin{cases} 2 > 0 \text{ loss} \\ 2 < 0, \text{ gain} \end{cases}$

$$\frac{I_t}{I_i} = \frac{A_t A_t^*}{A_i A_i^*} = \frac{(1-R)^2 G}{(1-GR)^2 + 4GR \sin^2(\frac{\theta}{2})} \quad (\text{homework})$$

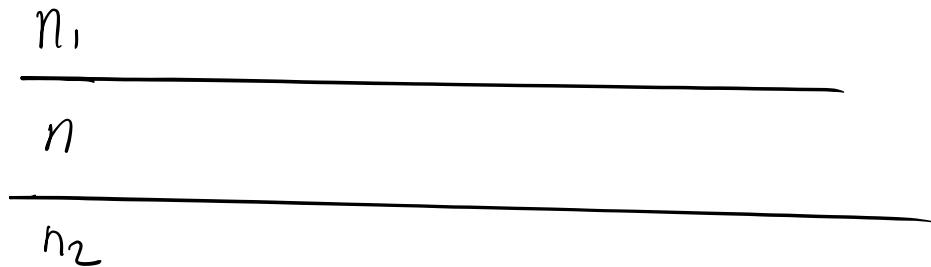
The maximum transmission

$$\left( \frac{I_t}{I_i} \right)_{\max} = \frac{(1-R)^2 G}{(1-GR)^2}$$



## 2. Asymmetric Fabry-Perot etalons. (P167, Yariv)

generic case:  $n_1 \neq n_2$



$$r = \frac{A_r}{A_i} = \frac{n_1 + (t_1 t_1' - r_1 r_1') r_2' e^{-i\delta}}{1 - r_1' r_2' e^{-i\delta}}$$

$$t = \frac{A_t}{A_i} = \frac{t_1 t_2' e^{-i\frac{\delta}{2}}}{1 - r_1' r_2' e^{-i\delta}}$$

Use the Stokes relationships  $\begin{pmatrix} tt^* + rr^* = 1 \\ tr'^* + rt^* = 0 \end{pmatrix}$  (HW)

$$T_{\text{etalon}} = \frac{A_t A_t^*}{A_i A_i^*} = \frac{(1-R_1)(1-R_2)}{(1-\sqrt{R_1} \sqrt{R_2})^2 + 4\sqrt{R_1} \sqrt{R_2} \sin^2(\phi)}$$

$$R_{\text{etalon}} = \frac{A_r A_r^*}{A_i A_i^*} = \frac{(\sqrt{R_1} - \sqrt{R_2})^2 + 4\sqrt{R_1} \sqrt{R_2} \sin^2(\phi)}{(1-\sqrt{R_1} \sqrt{R_2})^2 + 4\sqrt{R_1} \sqrt{R_2} \sin^2(\phi)}$$

$R_1, R_2$  are the reflectivity of interfaces,  $2\phi = \delta + \rho'_1 + \rho'_2$

$\rho'_1, \rho'_2$  are the phase shifts of reflections from interface 1 and interface 2, i.e.  $r'_1 = |r'_1| e^{-i\rho'_1}$ ,  $r'_2 = |r'_2| e^{-i\rho'_2}$

## Summary

① For lossless mirrors,  $R_1 + T_1 = 1$ ,  $R_2 + T_2 = 1$ ,

$$\Rightarrow T_{\text{etalon}} + R_{\text{etalon}} = 1$$

② When  $R_1 \neq R_2$ ,  $T_{\text{etalon}}$  cannot go to 1

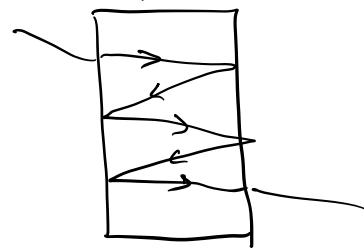
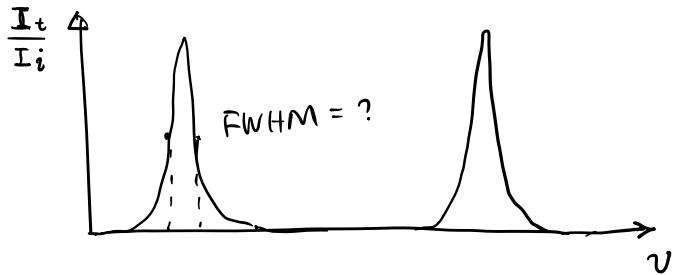
only when  $R_1 = R_2$  (symmetric F-P etalon),  $T=1$  can occur!

③ With gain/loss,  $G = \exp(-\alpha L)$

$$(T_{\text{etalon}})_{\max} = \frac{(1 - \sqrt{R_1})(1 - \sqrt{R_2})G}{(1 - \sqrt{R_1}\sqrt{R_2}G)^2}$$

## 3. Finesse, photon lifetime, Quality factor

① Finesse.



$$\frac{I_t}{I_i} = \frac{A_t A_t^*}{A_i A_i^*} = \frac{(1-R)^2}{(1-R)^2 + 4R \sin^2(\delta/2)} = \frac{1}{2}$$

$$\Rightarrow \sin^2\left(\frac{\delta - 2m\pi}{2}\right) = \frac{(1-R)^2}{4R}$$

Assuming the linewidth is small,  $\delta - 2m\pi \ll \pi$ ,

$$\Delta\delta_{1/2} = \frac{c}{2\pi n \lambda \cos\theta} (\delta_{1/2} - 2m\pi) \approx \frac{c}{2\pi n \lambda \cos\theta} \frac{1-R}{\sqrt{R}}$$

$$= \frac{FSR}{\frac{\pi\sqrt{R}}{1-R}}$$

$$= \frac{FSR}{F}$$

Define:  $F = \frac{FSR}{\Delta\delta_{1/2}} = \frac{\pi\sqrt{R}}{1-R}$  (Etalon Finesse) ①

Sources of cavity (etalon loss)

- ① Imperfection of reflection at mirrors
- ② Absorption and scattering loss in the medium between the mirrors.

round-trip reflection

$$R = r_1 r_2 \cdot \exp(-2\alpha_s l) = \exp(-2\alpha_{rl}) \quad (2)$$

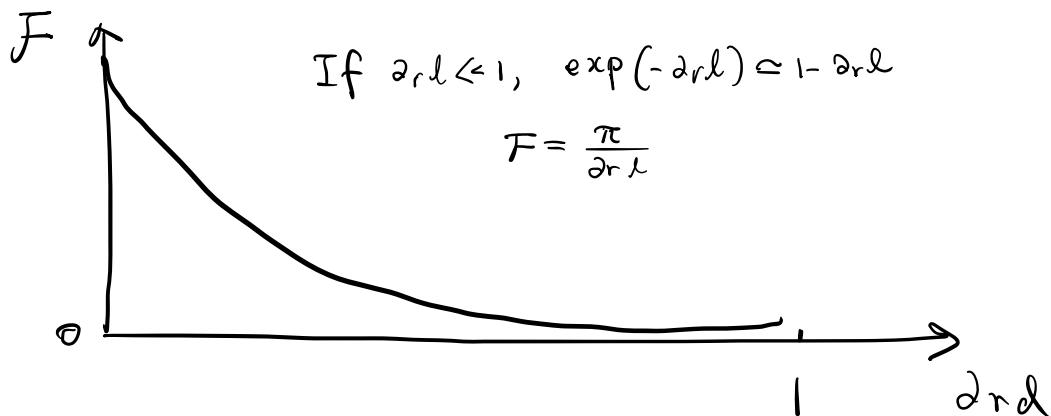
absorption loss      overall distribution loss  
unit: (cm<sup>-1</sup>)

$$\alpha_r = \alpha_s + \frac{1}{2l} \ln \frac{1}{r_1 r_2}$$

$$\begin{aligned}
 &= \alpha_s + \underbrace{\frac{1}{2l} \ln \frac{1}{n}}_{\text{loss of mirror 1}} + \underbrace{\frac{1}{2l} \ln \frac{1}{r_2}}_{\text{loss of mirror 2}} \\
 &= \alpha_s + \alpha_{m1} + \alpha_{m2}
 \end{aligned}$$

Plug in ② into ①;

$$F = \frac{\pi \exp\left(-\frac{\alpha_r l}{2}\right)}{1 - \exp(-\alpha_{rl})}$$



Summary:

① Finesse is defined as  $F = \frac{FSR}{\Delta\nu_{1/2}}$

② Finesse is a measure of cavity reflector loss and absorption/scattering loss in the etalon media.

③ Photon lifetime.

$$\Delta\nu_{1/2} = \frac{FSR}{F} \simeq \frac{c}{2n\lambda} / \frac{\pi}{\frac{\partial r}{\partial \lambda}} = \frac{c \frac{\partial r}{\partial \lambda}}{2\pi n} \\ \simeq \frac{1}{2\pi \tau_p}$$

④ Quality factor:

$$Q = 2\pi \cdot \frac{\text{stored energy}}{\text{energy loss per cycle}}$$

Stored energy  $E$ , loss rate:  $\frac{c}{n} \frac{\partial r}{\partial \lambda} E$ ,

loss per cycle:  $\frac{c \partial r E}{n \nu}$

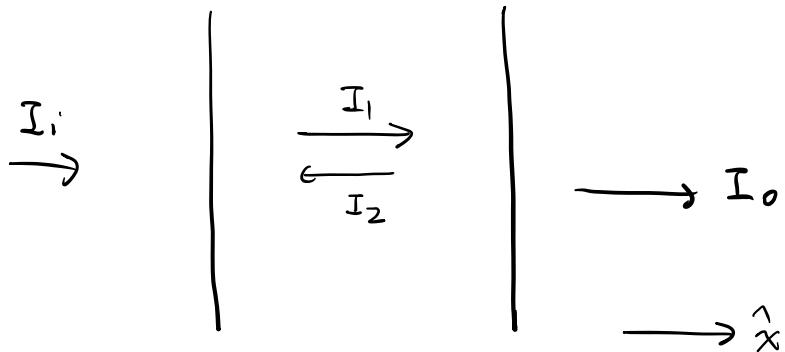
$$\Rightarrow Q = 2\pi \cdot \frac{E}{\frac{c \partial r E}{n \nu}} = \frac{2\pi n \nu}{c \partial r} \simeq \frac{\nu}{\Delta\nu_{1/2}}$$

It can also be shown that

$$Q \simeq \frac{v}{FSR} \cdot F$$

Usually,  $v \gg FSR$ ,  $Q \gg F$

## 4. Intracavity field



The  $\vec{E}$ -field inside cavity can be written as the sum of right traveling wave ( $I_1$ ) and left-traveling wave ( $I_2$ )

Assuming symmetric etalon:

$$I_o = \frac{(1-R)^2}{(1-R)^2 + 4R\sin^2(\frac{\delta}{2})} I_i$$

$$\left\{ \begin{array}{l} I_o = T \cdot I_1 = (1-R) I_1 \\ I_2 = R \cdot I_1 \end{array} \right.$$

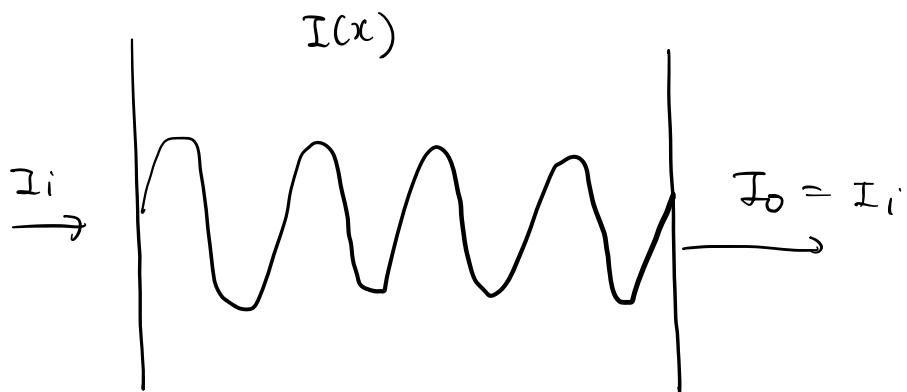
$$\Rightarrow I_1 = \frac{I_o}{1-R} = \frac{1}{1-R} I_i \quad \left. \begin{array}{l} \text{on resonance} \\ I_2 = \frac{R}{1-R} I_o = \frac{R}{1-R} I_i \end{array} \right\} \quad (1)$$

When on resonance, the right traveling and left traveling waves form an interference (standing wave) pattern inside the cavity:

intensity pattern ( $I(x)$ ) inside the cavity

$$I(x) = I_1 + I_2 + 2\sqrt{I_1 I_2} \cos(2kx + \phi_0) \quad (2)$$

On resonance (standing wave in cavity)



Plug in ① into ② and average,

$$I_{\text{avg}} = \frac{1+R}{1-R} I_i$$

If  $R = 0.99$ , when on resonance (standing wave is formed inside cavity),  $I_{\text{avg}}$  is 199 times higher than  $I_i$

What happens to the transmitted E-field?

The etalon transmission coefficient

$$t_e = \frac{A_e}{A_i} = \frac{T e^{-\frac{i\delta}{2}}}{1 - R e^{-i\delta}} \quad \underline{\phi = \frac{\delta}{2}} \quad \frac{T e^{-i\phi}}{1 - R e^{-2i\phi}}$$

$$= |t_e| e^{-i\psi}$$

phase shift of  
transmitted field

$$\psi = \phi + \tan^{-1} \left( \frac{R \sin 2\phi}{1 - R \cos 2\phi} \right)$$

the flight time (or group delay) of etalon

$$\tau_e = \frac{d\psi}{d\omega} = \frac{d\psi}{d\phi} \cdot \frac{d\phi}{d\omega} = \frac{d\psi}{d\phi} \cdot T \quad \begin{matrix} \Delta\phi = \omega \cdot \sigma t - k \cdot \alpha z \\ \sigma t = \frac{d\phi}{d\omega} \end{matrix}$$

single trip flight time  
(group delay)

When on resonance,  $\phi = \pi, 2\pi, 3\pi$

$$\frac{d\psi}{d\phi} = \left( \frac{1+R}{1-R} \right) \quad (\text{when } \phi = \pi, 2\pi, 3\pi)$$

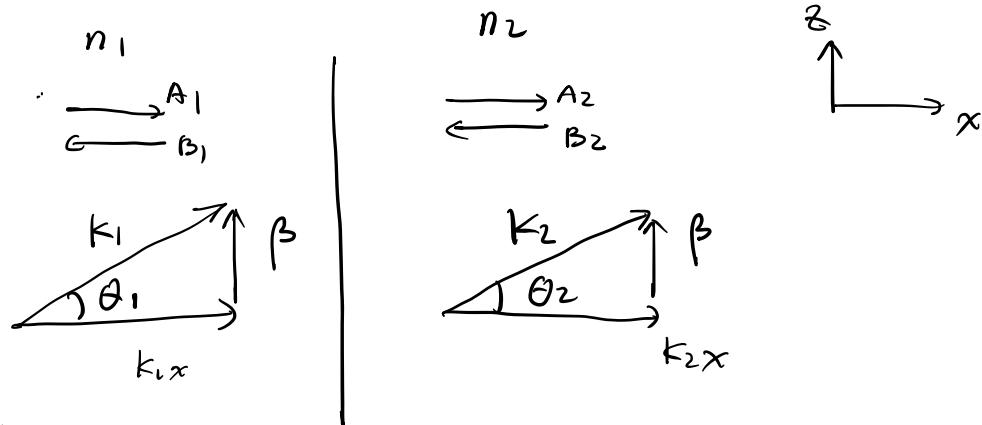
$$\text{So, } \tau_e = \left( \frac{1+R}{1-R} \right) T,$$

For  $R = 0.99$ , the time of flight (group delay) is enhanced by a factor of 199.

Summary :

## 5. Multicavity etalon and transfer matrix

### ① At interface



ignore int terms.

$$E = \begin{cases} (A_1 e^{-ik_1 x} + B_1 e^{ik_1 x}) e^{-i\beta z} & \text{medium 1} \\ (A_2 e^{ik_2 x} + B_2 e^{-ik_2 x}) e^{-i\beta z} & \text{medium 2} \end{cases}$$

$$\text{where } k_{1x}^2 + \beta^2 = k_1^2 = \left(n_1 \frac{\omega}{c}\right)^2$$

$$k_{2x}^2 + \beta^2 = k_2^2 = \left(n_2 \frac{\omega}{c}\right)^2$$

$$\begin{cases} B_1 = A_1 \cdot r_{12} + B_2 \cdot t_{21} \\ A_2 = A_1 \cdot t_{12} + B_2 \cdot r_{21} \end{cases}$$

where  $r_{12}, r_{21}, t_{12}, t_{21}$  are Fresnel reflection and transmission coefficients

$\Rightarrow$

$$A_1 = \frac{1}{t_{12}} A_2 - \frac{r_{21}}{t_{12}} B_2$$

$$B_1 = \frac{r_{12}}{t_{12}} A_2 + \left( t_{21} - \frac{r_{12} \cdot r_{21}}{t_{12}} \right) B_2$$

$$r_{21} = -r_{12},$$

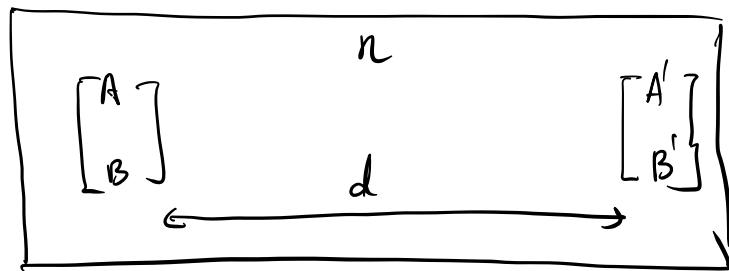
$$t_{12} t_{21} - r_{12} r_{21} = 1$$

$$\Rightarrow \begin{bmatrix} A_1 \\ B_1 \end{bmatrix} = \frac{1}{t_{12}} \begin{bmatrix} 1 & r_{21} \\ r_{12} & 1 \end{bmatrix} \begin{bmatrix} A_2 \\ B_2 \end{bmatrix} = T_{12} \begin{bmatrix} A_2 \\ B_2 \end{bmatrix}$$

transfer matrix

where  $T_{12}$  is defined as the transfer matrix between layer 1 and 2.  $T_{12}$  is asymmetric matrix.

② in homogeneous medium



propagation of plane wave in a homogeneous medium

$$\begin{bmatrix} A \\ B \end{bmatrix} = \begin{bmatrix} e^{i\phi}, & 0 \\ 0, & e^{-i\phi} \end{bmatrix} \begin{bmatrix} A' \\ B' \end{bmatrix} = P \begin{bmatrix} A' \\ B' \end{bmatrix}$$

↑ propagation matrix

phase shift is given by

$$\phi = k_x \cdot d = n \cdot \frac{\omega}{c} \cdot \cos \theta \cdot d.$$

If there are  $N+1$  media,

$$\begin{bmatrix} A_0 \\ B_0 \end{bmatrix} = \begin{bmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{bmatrix} \begin{bmatrix} A_{N+1} \\ B_{N+1} \end{bmatrix} \equiv M \begin{bmatrix} A_{N+1} \\ B_{N+1} \end{bmatrix}$$

where  $M = T_{01} \cdot P_1 \cdot T_{12} \cdot P_2 \cdots P_{N-1} \cdot T_{N-1} \cdot N \cdot P_N \cdot T_{N,N+1}$

$M_{21} = M_{12}^*$ ,  $M_{22} = M_{11}^*$  for lossless multilayer.

Determinant of M :

$$|M| = \frac{k_{n+1}x}{k_0x}$$

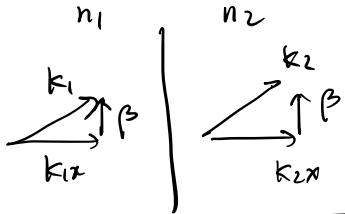
Recall that Fresnel coefficient :

$$r_{12} = \begin{cases} \frac{n_1 \cos \theta_1 - n_2 \cos \theta_2}{n_1 \cos \theta_1 + n_2 \cos \theta_2} &= \frac{k_{1x} - k_{2x}}{k_{1x} + k_{2x}} \quad (\text{s-wave}) \\ \frac{n_1 \cos \theta_2 - n_2 \cos \theta_1}{n_1 \cos \theta_2 + n_2 \cos \theta_1} &= \frac{n_1^2 k_{2x} - n_2^2 k_{1x}}{n_1^2 k_{2x} + n_2^2 k_{1x}} \quad (\text{p-wave}) \end{cases}$$

$$t_{12} = \begin{cases} \frac{2n_1 \cos \theta_1}{n_1 \cos \theta_1 + n_2 \cos \theta_2} &= \frac{2k_{1x}}{k_{1x} + k_{2x}} \quad (\text{s-wave}) \\ \frac{2n_1 \cos \theta}{n_2 \cos \theta_1 + n_1 \cos \theta_2} &= \frac{2n_1 n_2 k_{1x}}{n_1^2 k_{2x} + n_2^2 k_{1x}} \quad (\text{p-wave}) \end{cases}$$

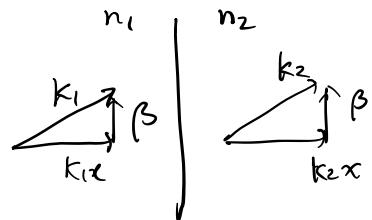
# Summary:

S-polarization



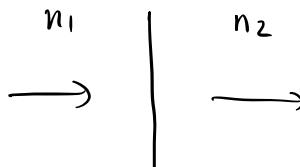
$$T_{12} = \frac{1}{2k_{1x}} \begin{bmatrix} k_{1x} + k_{2x}, & k_{1x} - k_{2x} \\ k_{1x} - k_{2x}, & k_{1x} + k_{2x} \end{bmatrix}$$

P-Polarization



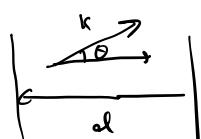
$$T_{12} = \frac{1}{2n_1 n_2 k_{1x}} \begin{bmatrix} n_1^2 k_{2x} + n_2^2 k_{1x}, & n_1^2 k_{2x} - n_2^2 k_{1x} \\ n_1^2 k_{2x} - n_2^2 k_{1x}, & n_1^2 k_{2x} + n_2^2 k_{1x} \end{bmatrix}$$

Normal incidence



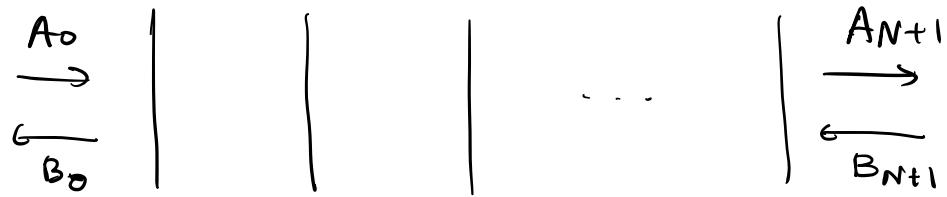
$$T_{12} = \frac{1}{2n_1} \begin{bmatrix} n_1 + n_2, & n_1 - n_2 \\ n_1 - n_2, & n_1 + n_2 \end{bmatrix}$$

Homogeneous media



$$P = \begin{bmatrix} e^{ik_x d} & 0 \\ 0 & e^{-ik_x d} \end{bmatrix}$$

Consider  $N+1$  layers and  $N$  interfaces.



$$\begin{bmatrix} A_0 \\ B_0 \end{bmatrix} = \begin{bmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{bmatrix} \begin{bmatrix} A_{N+1} \\ B_{N+1} \end{bmatrix} = M \begin{bmatrix} A_{N+1} \\ B_{N+1} \end{bmatrix}$$

where  $M = T_{01} P_1 \cdot T_{12} \cdot P_2 \cdot T_{23} \cdot P_3 \cdots P_{N-1} T_{N-1, N} \cdot P_N \cdot T_{N, N+1}$

$M_{21} = M_{12}^*$ ,  $M_{22} = M_{11}^*$  for lossless multilayer

Determinant of  $M$ :

$$\det(M) = \frac{k_{N+1} \omega}{k_0 \omega}$$

① If light is launched from the left side,  $B_{N+1} = 0$

$$A_0 = M_{11} A_{N+1}$$

$$B_0 = M_{21} A_{N+1}$$

total transmission / reflection coefficients:

$$t = \left( \frac{A_{N+1}}{A_0} \right) = \frac{1}{M_{11}}$$

$$r = \left( \frac{B_0}{A_0} \right) = \frac{M_{21}}{M_{11}}$$

② If light is launched from the right side;  $A_0 = 0$

$$t' = \left( \frac{B_n}{B_{n+1}} \right) = \frac{\det(M)}{M_{11}} \quad ①$$

$$r' = \left( \frac{A_{n+1}}{B_{n+1}} \right) = -\frac{M_{12}}{M_{11}} \quad ②$$

### Power transmittance

From left to right:  $T = \frac{k_{n+1}}{k_n} |t|^2$

right to left:  $T' = \frac{k_n}{k_{n+1}} |t'|^2$

plug in ①, ②., we have

$$\boxed{T = T'}$$